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Synopsis

Material transfer in underground mines often relies on ore and waste pass systems. Over the years the authors have investigated the design and performance of orepass systems in several Canadian and South African mines. It has been recognized that while most mining operations have either implicitly or explicitly clearly defined objectives, in the design and successfully operate orepass systems there seems to be an absence of a strategy on how to best attain these goals. Consequently, it is not surprising that the majority of operations reviewed by the authors experience a number of problems of varying degrees of severity and economic consequences. This is illustrated by reference to both South African and Canadian operations. The second part of this paper focuses on a review of tactical interventions to rectify orepass problems or mitigate their impact. The paper closes with a framework for a flexible strategy for the design and operation of orepass systems..

orepass; orepass design; orepass stability; orepass rehabilitation; orepass operation; orepass strategy.

Introduction

Most underground operations have relatively well defined strategies from the feasibility to the design stage. These include strategies for data collection and construction of geological and geomechanical models for the design and support of underground excavations. It is recognized, however, that vertical or nearvertical excavations, such as orepasses, are not given the same level of attention as horizontal

This paper draws from the experience of the authors in several mines and reaches the disappointing conclusion that there is an absence of strategy in orepass planning, design, and management. Consequently, it is not surprising that a large number of operations experience various problems of varying degrees of severity and economic consequences.

The case of orepass systems is somewhat complex as the major design decisions are often made at the early stages of design when there is often insufficient data. Further complications, specific to orepasses, lie in that it is not only necessary to maintain the stability of the excavation but also to ensure the noninterrupted transfer of material from one level to another.

Orepass system failures

System failure can be the result of any component failure. An orepass system is considered to have failed if it does not meet its required task of non-interrupted material flow for any given time. Orepass failures include failures along the wall due to geological structure, as shown in Figure 1, stress-related degradation resulting in orepass expansion (Figure 2), and erosion of the orepass such as in Figure 3. All these failures eventually lead to rehabilitation requirements.

The other types of observed orepass failures involve the interruption of material transfer. The transfer of coarse material can result in hang-ups due to interlocking arches, while the transfer of fine material results in hang-ups due to cohesive arches (Figure 4). Hang-ups due to cohesive arches are also associated with the use of cemented backfill. If flow is not restored there can be significant consequences for a mine. Restoring flow involves the use of a variety of techniques that can cause further damage to the orepass and are subject to their own set of safety concerns.

Another concern in orepass systems is the development of mud rushes or sudden inflows of mud. Butcher et al. (2005) suggest that the process originates with 'sticky' material formed from the fines and water adhering to the sides of an orerock pass or chute, impeding material flow and ultimately resulting in

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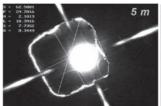
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Figure 1-Structural failures in orepasses



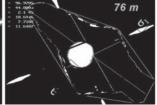


Figure 2—Stress-related degradation after a couple of months of use (20 kt of waste), after Goulet (2000)

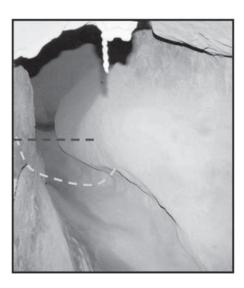


Figure 3-Rockpass wall wear condition after 6 years (6 Mt of ore)

blockage. Once a blockage or hang-up has occurred, further fines and water accumulating above the restriction provide the driving force for a mudrush when the chute is open or some disturbance of the blockage material occurs.

A successful strategy implies that the objectives in the planning, design, and operation of orepass systems are met. The corollary is that if the strategies are not fully successful they would be revised. This, however, contradicts the actual situation, where extensive reviews of both South African and North American mines report a series of documented failures.

In a study of more than 200 individual passes in South African deep-level gold mines, i.e. more than 2000 m, it was

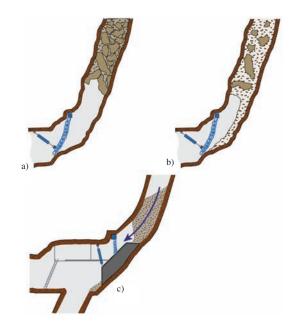


Figure 4—Hang-ups caused by (a) interlocking arches, (b) cohesive arches, and (c) mud rushes

observed that more than 50% of the passes had stability problems, and 16% had been abandoned (Joughin and Stacey, 2005a, b). The severity of the pass problem at deep level was illustrated by the fact that the maximum span of about 60% of the passes had doubled, or more, in size and that more than 20% of the passes had been abandoned. In Canada, based on data from over 20 mines, some type of material flow problems was reported at every site (Hadjigeorgiou *et al.*, 2005, 2008; Lessard and Hadjigeorgiou, 2006).

These failures transcend type of ore deposits, mining conditions, and company culture. An explanation is required to understand the numerous problems associated with orepasses. One interpretation would be that orepass system design and operation cannot be improved. This would be fatalistic and erroneous. Another explanation would be that the pursued strategies fail for a variety of reasons. The authors have reached the rather disappointing conclusion that in several cases orepass failures are preceded by the absence of strategy from the feasibility to the design and operational stage.

Tactical tools

Orepass management

The management of an orepass is a complex procedure and is often complicated by production considerations. The two major parameters in the successful operation of orepasses are whether it is necessary to restore flow using blasting, and whether the mine implements a cushion policy. Frequent blasting to restore flow and break up hang-ups or blockages can damage the orepass or chute. Experience suggests that orepasses kept full mitigate the damage associated with material hitting the walls. A further advantage of this practice is that it provides confinement to the sides of the pass, thus reducing structural failure or scaling due to high stress (Stacey and Swart, 1997).

A successful orepass management strategy requires a clear management structure and discipline. It was further observed that at some sites, orepasses are operated under a flow-through regime, even though there are guidelines against it. The usual explanations for these deviations from the site guidelines were that hang-up incidences require operators to keep muck levels lower than expected, and the need to 'keep feeding the mill'. It is easier for the operation to be more disciplined in keeping waste passes full given the higher priority in hoisting ore.

Material flow

The proper dimensioning of orepass systems is critical to ensure good material flow. An orepass should be dimensioned so as to avoid interlocking and cohesive hangups. Several guidelines are available to select these dimensions. The most reliable way to ensure that no oversize material enters an orepass is by use of appropriate block size infrastructure such grizzlies, mantles, and scalpers (Figure 5). Nevertheless, it has been difficult for some operations to invest in such infrastructure and at other places there is reluctance from workers to accept it, arguing that it slows down production.

Performance and monitoring

In comprehensive studies in South African and Canadian mines the authors recorded the lack of measurement, observation recording, and documentation of data on orepass system in mines. This is more surprising given that there are a variety of monitoring systems accessible (Table I). Since orepass systems are critical elements of the material handling system, the lack of quality quantitative data has hindered the development of robust predictors of orepass performance.

Liners

Liners have been proven as a useful tool to maintain the performance of ore- and waste pass systems as well as improving their longevity. Stacey and Swart (1997) suggest that the use of liners should be considered in weak rock or in fissile, scaling, or closely jointed blocky rock as a way to prevent uncontrolled growth of the pass dimensions. Liners are a plausible defence mechanism to protect the sides of the excavation from impact load. A liner system should provide impact resistance superior to the rock mass. In most cases, liners are installed as a preventive measure before commissioning the orepasses, but also as repair work to prolong the useful life of the orepass. Figure 6a is an example of a

successful use of abrasion-resistant shotcrete as a liner, while Figure 6b is a liner application that failed due to poor quality control.

Tactical interventions

Restoring flow

The transfer of coarse material can result in hang-ups due to interlocking arches, while the transfer of fine material results





a) Grizzly

b) Scalper



c) Mantle

Figure 5—Block size control infrastructure: (a) grizzly, (b) scalper, and (c) mantle

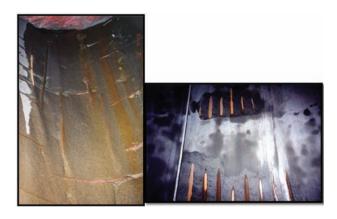


Figure 6—(a) Successful application of abrasion-resistant shotcrete liner in a vertical (storage) silo; photo after 7 years in operation (10 Mt) and (b) poor quality control during application whereby shotcrete was not allowed to cure, resulted in excessive wear of shotcrete and rails

Table I Muck level monitoring systems in Canadian orepasses, after Hadjigeorgiou et al. (2005)					
Туре		Comments			
Direct	Visual	Evaluation of the muck level is performed periodically by supervising personnel. Inaccurate. Cannot be automated			
	Measuring tape	A weighted tape is used by supervising personnel to periodically record the muck level. Cannot be automated Laser systems can provide real-time muck level readings Very accurate. Can be automated. High capital cost			
	Laser	Sensitive to dust			
Indirect	Tonnage reconciliation	Subtracting pass capacity and pass output to pass input (scoop buckets). Highly inaccurate			

in hang-ups due to cohesive arches. Blockages are localized in the vicinity of the chute, while hang-ups are found in the orepass. If flow is not restored there can be significant consequences for the operation.

Table II lists the various methods employed to restore flow, with varying rates of success, in Canadian mines. Figure 7 provides a matrix that can be used to identify the most appropriate technique to apply in order to restore flow in an orepass system. The first consideration depends on the type of a hang-up or blockage, such as cohesive, interlocking, or large single boulders, that is observed. The next criterion is the location of the hang-up, i.e. whether it is at the chute or higher up in the orepass. Recommendations are then based on whether a particular strategy is pertinent or whether it can

be used, but with a certain degree of caution. Several methods are simply not recommended.

Rehabilitation

Rehabilitation of orepass systems is very costly and usually involves supporting an orepass under what can be extremely challenging and often dangerous conditions. Rehabilitation efforts can be undertaken either from outside or from inside, with the advantages and limitations of each approach summarized in Table III.

As a general rule, rehabilitation from inside a pass is dangerous, as it exposes workers to hazardous conditions. Any type of rehabilitation is expensive, whether the costs are direct or indirect. Depending on the type of rehabilitation

Table II Methods employed in Canadian mines to restore flow in ore passes				
Category	Methods to restore flow			
Methods that employ water	Introduction of water from above the hang-up or blockages Introduction of water from a point below the blockage			
Explosive-based methods	Close range drilling and use of explosive Drilling from a distance and use of explosives Use of 'Sputnik' Use of blasting poles			
Mechanical methods	Use of rock breakers to break down large boulders wedged at the tipping point			

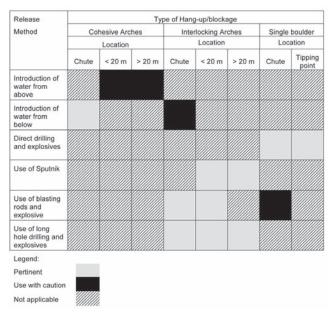


Figure 7—Applicability of different methods to restore material flow in ore and waste passes

Table III Advantages and limitations of rehabilitation techniques, after Mercier-Langevin and Hadjigeorgiou (2004)					
Rehabilitation techniques	From inside	From outside			
Advantages	Any type of support can be installed Any type of liner can be installed Good understanding of the failure mechanism	Production can carry on as usual Safe for personnel			
Limitations	The pass has to be emptied and production stopped Unsafe for personnel	Only cable bolts can be installed Liners cannot be installed Poor understanding of the initial failure mechanism			



Figure 8-Examples of orepass rehabilitation work

performed on the pass, production may have to be stopped. In the case of a major orepass, this can mean production stoppage for the entire mine. Figure 8 illustrates examples of the effort required in the rehabilitation work in orepasses.

The actual costs of rehabilitating passes are extremely high when compared with the initial cost of development. If one considers the stops in production during the rehabilitation then the costs can be staggering. This would imply that there is a need of a rehabilitation strategy at the early stages of design. Although it may be difficult to present at the feasibility stage, there is a case to be made for planning rehabilitation, and there is a case for planning replacement passes to be developed simultaneously with the planned passes.

Towards an orepass system strategy

An orepass strategy would aim to ensure that an orepass system operates at its design performance throughout its design life. A well thought out strategy would employ a series of tactics or tools to ensure this objective. Arguably, every mining company enjoys its own operating philosophy that invariably influences the design and operation of a mine. It would be a logical extension that this approach may be applied in the development of coherent strategies that would consider expectations from mine management, engineering, and underground supervisory personnel on the design and operation of orepass systems. If such strategies were successful then the number of system failures would be difficult to explain. This section provides a template for a successful strategy in the planning, design, and operation of orepass systems.

Tactical mistakes

A review of several mining operations in Canada and South Africa has identified the following tactical errors that have

resulted in multitude of problems in the operation of orepass systems (Table IV). It can be argued that these errors can and should be avoided.

As shown in Table IV, these tactical errors have as much to do with human resources as operational resources. The only way for a strategy to succeed is for the company to establish both clear objectives and responsibilities that lead to an integrated approach engaging all the stakeholders at every part of the process.

Strategy at the design stage

Stacey (2004) has been a strong proponent of the design process as defined by Bieniawski (1992), and has illustrated that these design principles are readily adaptable to orepass design. This section provides a flexible strategy that can be implemented at any site.

Design principle 1: Clarity of design objectives and functional requirements

A statement of the 'problem' and a statement of the design objectives to satisfy this problem, taking account of any constraints that are present, is essential to any design process. In orepass design, for example, it is necessary to establish whether the mine aims to operate a single or a dual system, whether it will be operated with cushion guidelines (storage) or as flow-through, located near the shaft or the orebody, etc.

Design principle 2: Minimum uncertainty of geological conditions

The orepasses will be excavated in rock masses which can be very variable. In efforts to control costs it is not unusual to limit geotechnical investigations, with the result that geological conditions are often unknown or, at best, little known. A structural model will ensure that the orepasses are placed away from major geological structures. Drilling pilot holes in the preferred location for each segment of the system can allow the assessment of rock mass quality and provide data for the geotechnical assessment such as the Q system by Barton et al. (1974) and the RMR system by Bieniawski (1989). Reliable classification records for the site can ensure that areas where the rock mass quality is poor (Q < 5, RMR)< 60) are avoided. The minimization of uncertainty can result in more confident design and reduction of risk. An area that seems to be often overlooked is establishing the properties of transferred material in an orepass. Quite often there is

Table IV							
Tactical errors relating to the design and operation of ore pass systems							
Type of tactical error	Example	Frequency					
Absence of clear objectives	Absence of integrated approach to account for operational, material and stability elements concerns; isolated design elements	More common at feasibility stage					
Inadequate data collection	Absence of pilot holes	More common at feasibility stage					
Lack of detailed engineering	Focusing on stability and ignoring material flow	Frequent at the design stage					
Control mechanisms	Absence of control chains	Frequent at the design stage					
Management	Ownership and accountability of orepass management	Common at the operation level					

inadequate information on critical properties such as particle size distribution, angle of repose, angle of friction, and mineral composition.

Design principle 3: Simplicity of design components

An important step in the design of a rockpass is the development of a geotechnical model. This may be conceptual, but it is important to be able to describe the likely behaviour of the rock mass in which the pass is located and the possible mechanisms of instability. Only once this has been done can appropriate design (failure) criteria be decided on, design limits be defined, required factors of safety or probabilities of failure be defined, a design model (or models) be developed, and appropriate design analysis methods be decided upon. This will ensure that the design is appropriate, and as simple as possible.

Design principle 4: State-of-the-art practice

The implication of this principle is that up-to-date concepts, analyses, and methods must be used whenever they are appropriate. There are several developments in the engineering toolbox that can be used. These include sophisticated 3D stress analysis modelling (Figure 9).

Further tools include a range of design guidelines, for example Fergusson (1991), Stacey and Swart (1997), Beuss *et al.* (2001), Mercier-Langevin and Hadjigeorgiou (2004). Furthermore, Brummer (1998) as well as Hadjigeorgiou and Mercier-Langevin (2008) proposed quantitative methodologies that can be used to establish the projected longevity of orepass systems, based on ground and stress conditions, impact loads on the walls of the orepass, installation of suitable support, and the implementation of proper orepass management techniques.

Design principle 5: Optimization

Risk integrally involves numerous factors including safety, cost, productivity, seismicity, water, manpower, etc.

Therefore, to minimize risk, designs must be optimized. An optimized design will result from the evaluation of the output from alternative designs. This would involve a trade-off study of the available design choices for orepasses. An example of optimized design in deep mines is the development of a redundant orepass, which can then be used during maintenance of the principal ore- and waste passes. This would ensure that there is no disruption to production.

Design principle 6: Constructability

If the design cannot be implemented safely and efficiently it does not satisfy the principle of constructability and therefore is not optimized.

Conclusions

The argument that most mines do not have a strategy in planning, designing, and operating orepass systems appears to be somewhat extreme. The fact that there are so many orepass problems would argue that this is in fact true, or at best the developed strategies are not successful. This raises the question why this is so.

A plausible explanation is that the financial costs of failed strategies have not been recognized. In the absence of documentation on hang-up frequency and production costs the information is not readily available to the decision-makers.

Although most mines can quantify very well the construction costs and the 'normal' operational (chute and rock breaker operation) and maintenance (chute and grizzly) costs, they do not have comprehensive data on what one may refer to as 'irregular' costs such as hang-up clearing, rehabilitation, repairing blast damage to chutes, etc. It is these 'irregular' cost that result in production losses, which is the single most important economic factor to consider.

An extreme example of the significance of orepass systems is provided in Figure 10 from an underground gold mine. In this case, the expansion of the orepass resulted in extensive production losses. This case is of particular interest in that the orepass was at an unfavourable orientation to the

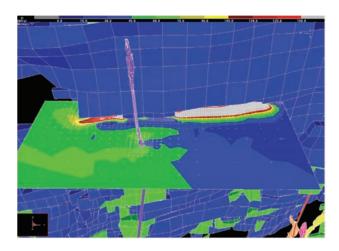


Figure 9—Map3D stress analysis of induced stress conditions around the 1000 SFR orepass at Brunswick Mine, after Hadjigeorgiou *et al.* (2008)

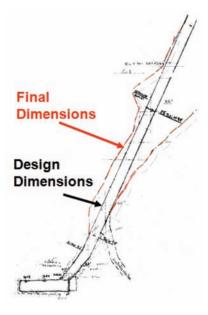


Figure 10—Failed orepass, where the expansion of the orepass resulted in severe production losses

prevalent geological structure, thus aggravating the situation. Another example that demonstrates the costs of lack of strategy is from a nickel mine, where the mine had no alternative but to rehabilitate a critical orepass using a liner. The actual costs of the rehabilitation orepass were close to C\$7 million.

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Erratum

Correct Figure 12

Figure 12 which was printed in the Rogers paper in the SAIMM Journal in July 2013 entitled, 'KX36-rediscovering the diamond exploration potential of the central Kalahari in Botswana', by A.J. Rogers, T.G. Hough, and J.M. Davidson, vol, 113, no 7, pp. 539-545 was incorrectly printed.

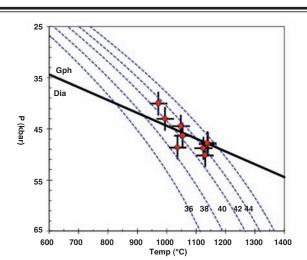


Figure 12-Nimis and Taylor thermobarometry results for peridotitic CPX from KX36. Model geotherms are from Pollack and Chapman (1977). Graphite/diamond stability curve is from Kennedy and Kennedy (1976)